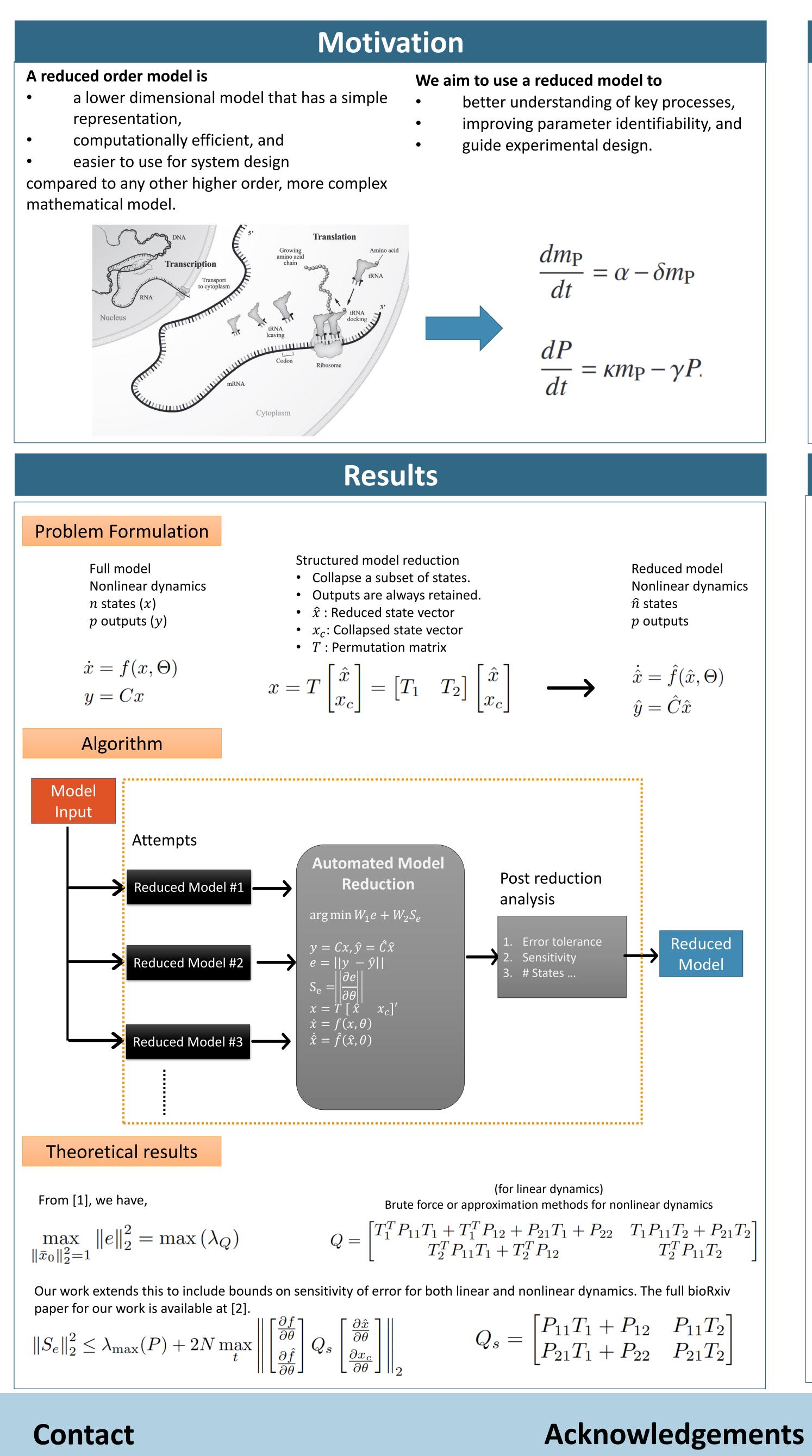
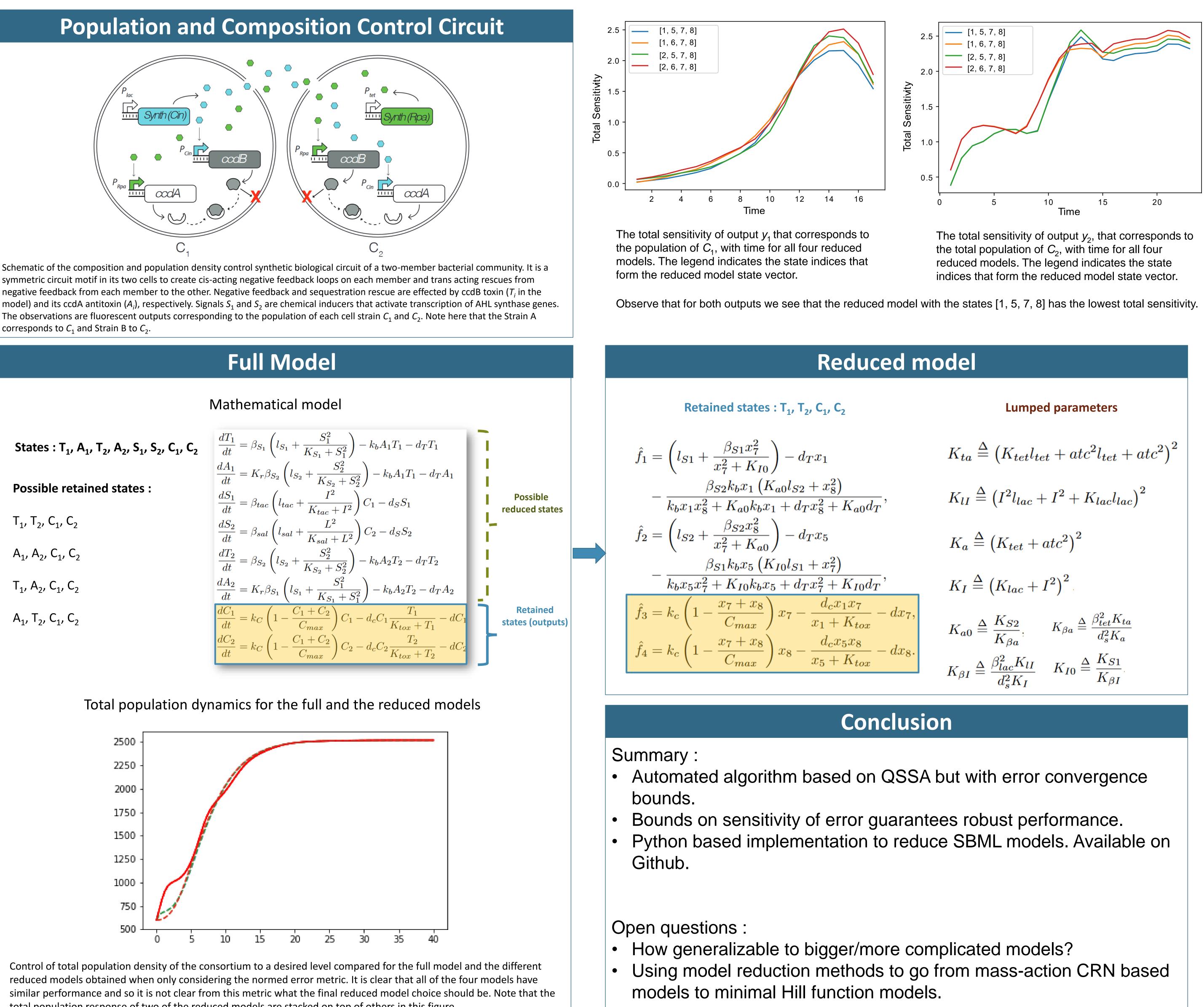
Caltech

An automated model reduction tool to guide the design and analysis of synthetic biological circuits



Ayush Pandey California Institute of Technology Email : apandey@caltech.edu

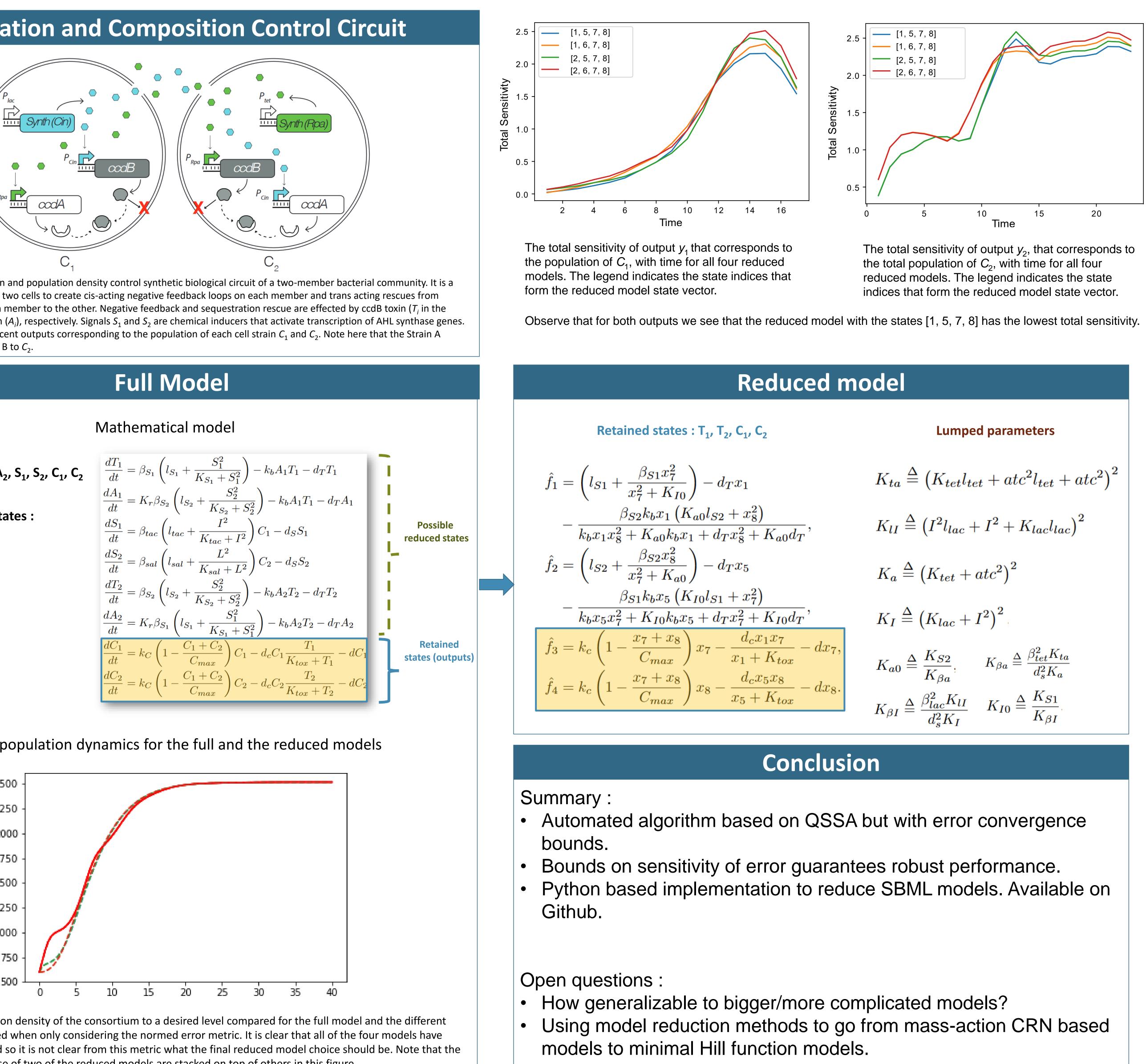
Ayush Pandey¹; Richard M. Murray¹ ¹Control and Dynamical Systems, California Institute of Technology



corresponds to C_1 and Strain B to C_2 .

States : T_1 , A_1 , T_2 , A_2 , S_1 , S_2 , C_1 , C_2 **Possible retained states :** T₁, T₂, C₁, C₂ A₁, A₂, C₁, C₂

$$\frac{dT_1}{dt} = \beta_{S_1} \left(l_{S_1} + \frac{S_1}{K_{S_1}} \right)$$
$$\frac{dA_1}{dt} = K_r \beta_{S_2} \left(l_{S_2} + \frac{S_1}{K_1} \right)$$
$$\frac{dS_1}{dt} = \beta_{tac} \left(l_{tac} + \frac{S_1}{K_{tac}} \right)$$
$$\frac{dS_2}{dt} = \beta_{sal} \left(l_{sal} + \frac{S_1}{K_{sa}} \right)$$
$$\frac{dT_2}{dt} = \beta_{S_2} \left(l_{S_2} + \frac{S_2}{K_{S_2}} \right)$$
$$\frac{dA_2}{dt} = K_r \beta_{S_1} \left(l_{S_1} + \frac{S_1}{K_1} \right)$$
$$\frac{dC_1}{dt} = k_C \left(1 - \frac{C_1 + C_1}{C_{max}} \right)$$
$$\frac{dC_2}{dt} = k_C \left(1 - \frac{C_1 + C_1}{C_{max}} \right)$$



total population response of two of the reduced models are stacked on top of others in this figure.

We would like to thank Chelsea Hu for the population control circuit figure used. The project or effort depicted was or is sponsored by the Defense Advanced Research Projects Agency (Agreement HR0011-17-2-0008). The content of the information does not necessarily reflect the position or the policy of the Government, and no official endorsement should be inferred.

References

- 1. Antonis Papachristodoulou et al. "Structured model reduction for dynamical networked systems." 49th IEEE Conference on Decision and Control (CDC). IEEE, 2010, pp. 2670–2675.
- 2. Ayush Pandey and Richard M. Murray. "An automated model reduction tool to guide the design and analysis of synthetic biological circuits." *bioRxiv* (2019): 640276.

$$\hat{f}_{1} = \left(l_{S1} + \frac{\beta_{S1}x_{7}^{2}}{x_{7}^{2} + K_{I0}}\right) - d_{T}x_{1}$$

$$- \frac{\beta_{S2}k_{b}x_{1}\left(K_{a0}l_{S2} + x_{1}\right)}{k_{b}x_{1}x_{8}^{2} + K_{a0}k_{b}x_{1} + d_{T}x_{8}^{2}}$$

$$\hat{f}_{2} = \left(l_{S2} + \frac{\beta_{S2}x_{8}^{2}}{x_{7}^{2} + K_{a0}}\right) - d_{T}x_{8}$$

$$- \frac{\beta_{S1}k_{b}x_{5}\left(K_{I0}l_{S1} + x_{1}\right)}{k_{b}x_{5}x_{7}^{2} + K_{I0}k_{b}x_{5} + d_{T}x_{7}^{2}}$$

$$\hat{f}_{3} = k_{c}\left(1 - \frac{x_{7} + x_{8}}{C_{max}}\right)x_{7} - \frac{d_{1}x_{1}}{x_{1}}$$

$$\hat{f}_{4} = k_{c}\left(1 - \frac{x_{7} + x_{8}}{C_{max}}\right)x_{8} - \frac{d_{1}x_{5}}{x_{5}}$$



Caltech

_L , C ₂	Lumped parameters
L	$K_{ta} \stackrel{\Delta}{=} \left(K_{tet} l_{tet} + atc^2 l_{tet} + atc^2 \right)^2$
$\frac{x_8^2}{+K_{a0}d_T},$	$K_{lI} \stackrel{\Delta}{=} \left(I^2 l_{lac} + I^2 + K_{lac} l_{lac} \right)^2$
5	$K_a \stackrel{\Delta}{=} \left(K_{tet} + atc^2 \right)^2$
$\left(\frac{x_7^2}{+K_{I0}d_T}, \frac{1}{x_1x_2}\right)$	$K_I \stackrel{\Delta}{=} \left(K_{lac} + I^2 \right)^2$
$\frac{l_c x_1 x_7}{+ K_{tox}} - dx_7,$ $l_c x_5 x_8$	$K_{a0} \stackrel{\Delta}{=} \frac{K_{S2}}{K_{\beta a}}, \qquad K_{\beta a} \stackrel{\Delta}{=} \frac{\beta_{tet}^2 K_{ta}}{d_s^2 K_a}$
$\frac{l_c x_5 x_8}{+K_{tox}} - dx_8.$	$K_{\beta I} \stackrel{\Delta}{=} \frac{\beta_{lac}^2 K_{lI}}{d_s^2 K_I} K_{I0} \stackrel{\Delta}{=} \frac{K_{S1}}{K_{\beta I}}$